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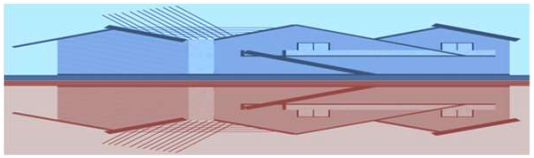
Building Integration of Solar Thermal Systems – TU1205 – BISTS

Hybrid Photovoltaic/Thermal Collectors



Prof. Yiannis Tripanagnostopoulos

Univ. of Patras, Patra, Greece

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Photovoltaics and temperature aspects

The conversion rate of solar radiation into electricity by photovoltaics depends on cell type and is between 5%-25%.

The greater part of the absorbed solar radiation by photovoltaics is converted into heat (at about 60%-70%), increasing cell temperature.

This effect reduces their electrical efficiency - mainly to silicon cells - and is an essential difference between solar thermal collectors and photovoltaics, for the required conditions for their effective operation.

The solar thermal collectors aim to achieve higher absorber temperature, in order to provide heat removal fluid efficiently and at higher temperature, while the PV cells operate in lower temperatures in order to achieve higher efficiency in electricity.

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Photovoltaics are mainly made from silicon semiconductors, based on monocrystalline silicon (c-Si) , polycrystalline silicon (pc-Si) and amorphous silicon (a-Si) modules.

In terrestrial applications, the pc-Si type PV modules are the most widely applied among silicon type photovoltaics, followed by cadmium telluride (CdTe) and copper indium gallium selenide CIGS, while new types of photovoltaics, as of dye-sensitized solar cells (DSSCs), have been investigated.

Silicon type photovoltaics are still the main cell types in applications because they have longer durability and higher efficiency than other photovoltaics.

The photovoltaics based on other than silicon materials (CdTe, CIGS, DSSCs, etc), would follow in applications next years and mainly in the built sector.

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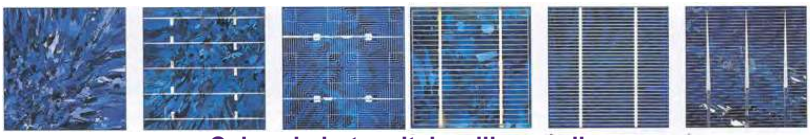
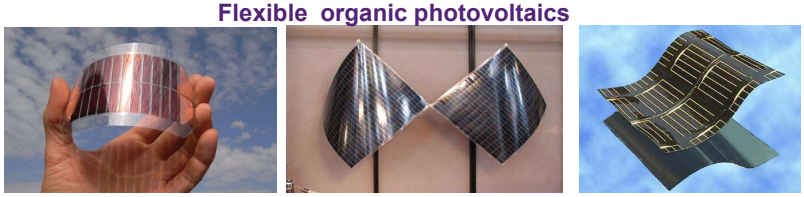
Photovoltaics

Typical silicon photovoltaic cells



Colored photovoltaic silicon cells

Flexible organic photovoltaics



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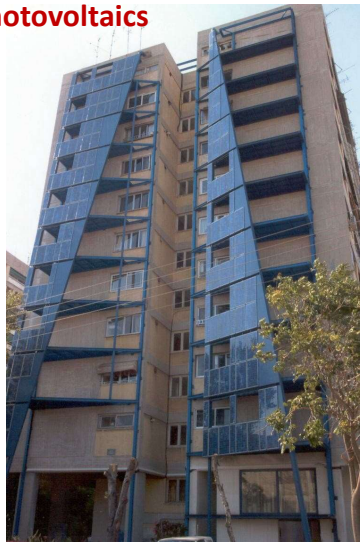
Photovoltaics



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In case of PV modules that are installed in parallel rows on horizontal plane of ground or building roof, the exposure of both PV module surfaces to the ambient permits their natural cooling.

In façade or inclined roof installation on buildings the thermal losses are reduced due to the thermal protection of PV rear surface and PV modules operate at higher temperatures. This undesirable effect can be partially avoided by applying a suitable heat extraction with a fluid circulation, air or liquid (water), keeping the electrical efficiency at a satisfactory level.

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The hybrid Photovoltaic/Thermal (PV/T or PVT) collectors are the solar energy systems that consist of PV modules combined with thermal units and provide simultaneously electricity and heat. PV/T collectors are mainly of flat type in form and are distinguished in water cooled (PV/T-water) and air cooled (PV/T-air) collectors.

PV/T collectors can be applied to buildings, instead of separate solar thermal and photovoltaics

In addition, there have been developed concentrating PV/T collectors (CPV/T), using reflectors or lenses and a circulating fluid to avoid higher PV operating temperatures, due to the concentrated solar radiation on cells.

Hybrid PV/T systems can be used for the production of electricity and heat to residential and office buildings, hotels, hospitals, athletic centers, industries and to agricultural applications.

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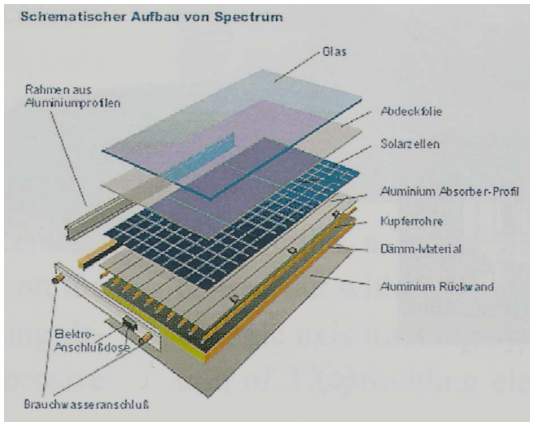
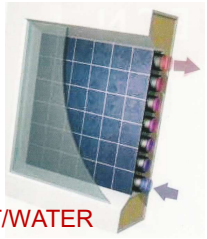
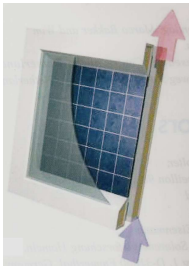
Hybrid Photovoltaic/Thermal Solar Energy Systems





PVT/WATER



PVT/AIR

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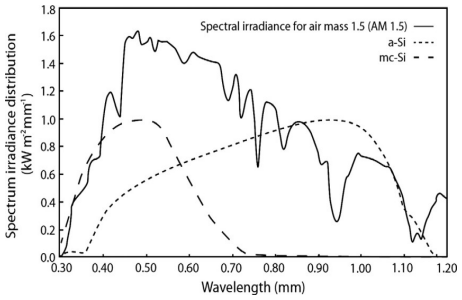
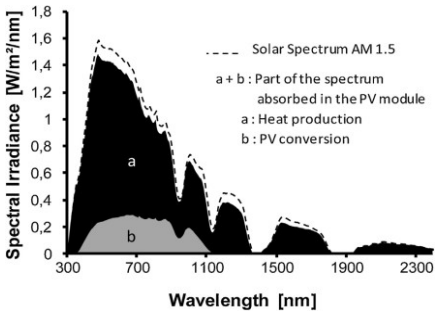


(from Aste et al, 2014)



(from Dupeyrat et al, 2014)

Spectral solar radiation absorption response of crystalline and amorphous silicon cells and the conversion rates for heat and electricity

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History of PV/T (1st period 1975-2000)

The first step on PV/T collectors is the works of Wolf (1976) and Kern and Russell (1978), for the design and performance of water and air cooled PV/T systems.

Following, are the studies of Hendrie (1979) , Florschuetz (1979) and Cox and Raghuraman (1985). PV/T collectors for building integration: Sopian et al (1996), Garg and Adhikari (1997), Brinkworth et al (1997), Moshfegh and Sandberg (1998), Schroer et al (1998), Brinkworth (2000).

Eicker et al (2000) give monitoring results from a BIPV/T system and Bazilian et al (2001) evaluate the practical use of several PV/T systems with air heat extraction in the built environment.

Applications of PV/T-air systems have been given by Chow (2003), Hegazy (2000), Ito with Miura (2003), Infield et al (2004), Charron and Athienitis (2006), Brinkworth and Sandberg (2006).

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History of PV/T (1st period 1975-2000)

Some of the most important first studies on PV/T-Water systems is the work of Bergene and Lovvik (1995) for detailed analysis on liquid type PVT systems, of Elazari (1998) for design, performance and economic aspects of commercial type PV/T water heater, Hausler and Rogash (2000) for a latent heat storage PVT system and of Kalogirou (2001), with TRNSYS study for PVT-Water systems.

Later, Huang et al (2001) presented a PV/T system with hot water storage and Sandness and Rekstad (2002) gave results for PVT collectors with polymer absorber.

Dynamic 3D and steady state 3D, 2D and 1D models for PV/T –Water have been studied and presented by Zondag et al (2002, 2003).

Experimental results on PV/T-Water and PV/T-Air systems, including the use of diffuse reflectors, were published by Tripanagnostpoulos et al (2002, 2007).

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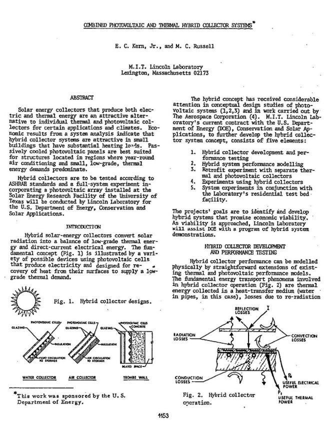


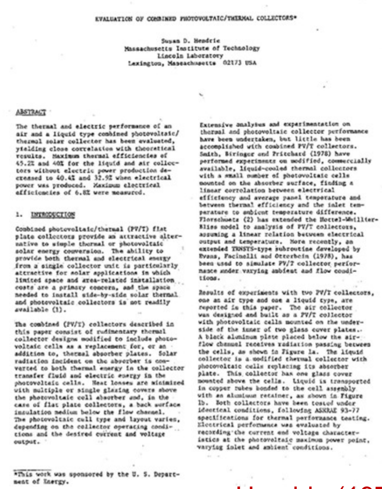
COMBINED PHOTOVOLTAIC AND THERMAL HYBRID COLLECTOR SYSTEMS*

E. C. Kern, Jr., and M. C. Russell

M.I.T. Lincoln Laboratory
Lexington, Massachusetts 02173

Kern and Russell (1978)

13th IEEE Photovoltaic Specialists, Washington , 1978



EVALUATION OF COMBINED PHOTOVOLTAIC/THERMAL COLLECTORS*

Susan D. Hendrie
Massachusetts Institute of Technology
Lincoln Laboratory
Lexington, Massachusetts 02173 USA

Hendrie (1979)

ISES Conf., Atlanta, 1979

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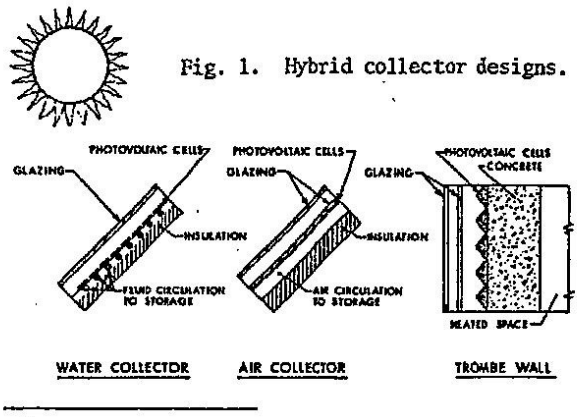

Kern and Russell (1978)
13th IEEE Photovoltaic Specialists, Washington , 1978

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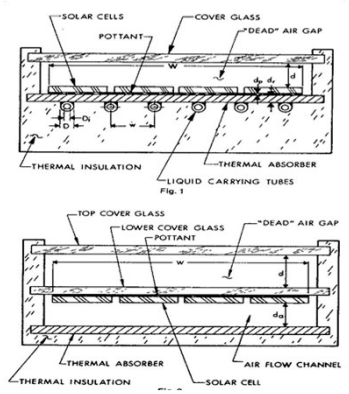
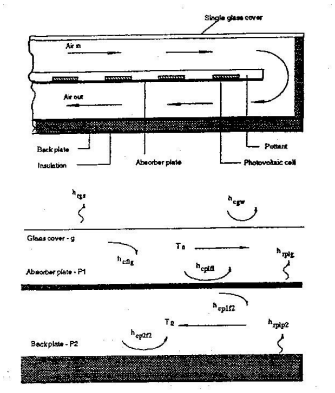


Bhargava et al (1991),



Sopian et al (1996)

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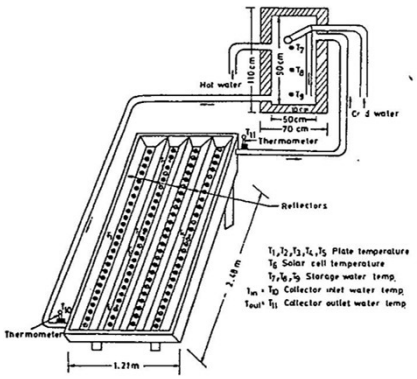
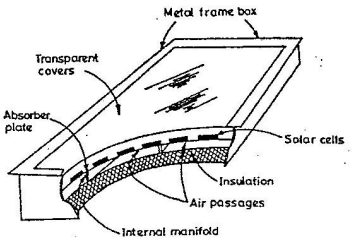


Garg and Agarwal (1995)

Garg and Adhikari (1997)



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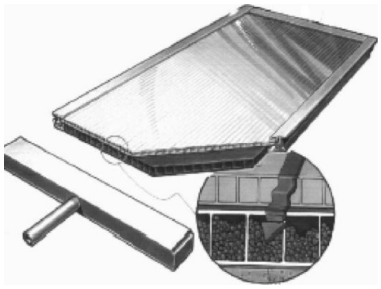
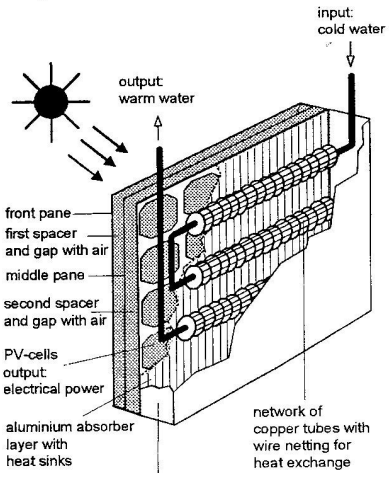
Sandness and Rekstad (2002)





Hausler and Rogash (2000)

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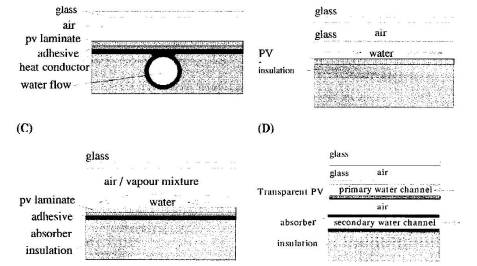
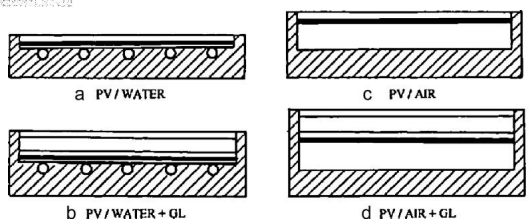


Zondag et al (2002)



Tripanagnostopoulos et al (2002)

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History of PV/T (2nd period 2000-2015)

Following, among other works are: PV/T modelling by Chow (2003), Ji et al (2003), Notton et al (2005), PV/T-water prototypes by Busato et al (2008), domestic PV/T systems by Coventry and Lovegrove (2003) and performance/cost results of a roof PV/T system by Bakker et al (2005).

In addition, there are: the theoretical approach for domestic heating and cooling with PV/T collectors by Vokas et al (2006), performance evaluation by Tiwari and Sodha (2006), floor heating by Fraisse et al (2007) and heat pump PV/T by Fang et al (2010).

Works on thermosiphonic PV/T systems have been performed by Kalogirou (2001), Chow and He (2006), Kalogirou & Tripanagnostopoulos (2006).

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History of PV/T (2nd period 2000-2015)

Works on ventilated building PV facades were also performed by Guiavarch and Peuportier (2006), Charron and Athienitis, (2006) and Brinkworth and Sandberg (2006). Some studies on improved PV/T-air collectors were published by Tonui and Tripanagnostopoulos (2007, 2008), a detailed study using CFD methodology for air cooled photovoltaics was presented by Gan (2009) and the performance of a building integrated PV/T collector was published by Anderson et al (2009).

The energy performance for three PV/T configurations for a house (Pantic et al, 2010) gives interesting information and the effective use of PV/T-air collectors for buildings with life cycle cost analysis (Agrawal and Tiwari, 2010), shows the difference in using c-Si and a-Si PV modules to buildings.

Last years, the works of Mazon et al (2011), Dupeyrat et al (2011, 2014), Ibrahim et al (2011), Ciulla et al (2012), J.H Kim and J.T. Kim (2012), Aste et al (2012, 2014), Helmers and Kramer (2013), Kramer and Helmers (2013), Fortuin et al (2014), Touafek et al (2014) and also Matuska (2014) could be referred.

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History of PV/T (concentrating PV/T)

PV modules should be kept at low temperatures to result satisfactory electrical efficiencies. This requirement limits PV/T effective operation to low temperatures, although temperatures up to 60 ^{o}C - 70 ^{o}C can be achieved.

To obtain effective fluid temperature at higher level, PV/T collectors with lower thermal losses for higher thermal efficiency or CPV/T collectors, could be used. CPV/T collectors are of flat, CPC, PTC and Fresnel type reflectors or lenses.

In CPV/T systems PV cooling is needed because the absorbed concentrated radiation results to higher cell temperatures. In that case the circulating heat removal fluid can be heated to a considerable temperature level for practical applications.

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History of PV/T (concentrating PV/T)

Regarding dielectric lens-type concentrators, optical results show that for 3D static acrylic lens concentrators, a reduction of 62% in cell surface is achieved (Yoshioka et al, 1997, Zacharopoulos et al., 2000, Shaw and Wenham, 2000).

In medium concentration photovoltaics, 2D concentrators have been applied, with most known being the Eucledes system (Luque et al, 1998), consisted of a parabolic trough reflector and flat type absorber of PV cell strips on focal line.

In the 3D CPV systems, the Fresnel lenses is the majority of the used concentrating optical media with less applied the concentrators of reflector type (Ries et al., 1997, Rumyantsev et al., 2000, Lorenzo and Sala, 1979, O'Neil et al., 2000, Bottenberg et al., 2000, Kritchman et al, 1979).

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History of PV/T (concentrating PV/T)

Concentrating photovoltaics are more sensitive than thermal collectors to the density of solar radiation on the absorber surface and a homogenous radiation distribution is necessary, to avoid reduction of the electrical output from the cells.

Flat or CPC type reflectors combined with PV/T collectors have been proposed by Garg and Adhikari (1999), Brogren et al (2000, 2002), Karlsson et al (2001), Tripanagnostopoulos et al (2002), Othman et al (2005), Mallick et al (2007), Nilsson et al (2007), Robles-Ocampo et al (2007) and Kostic et al (2010).

Works on CPV/T systems with linear parabolic reflectors are by Coventry (2005), linear Fresnel reflectors by Rossel et al (2005), compound reflectors by Tyukhov et al (2009), linear Fresnel lenses by Tripanagnostopoulos et al (2006), by Chemisana and Ibanez (2010) and point focus paraboloidal dish reflector by Helmers and Kramer (2013).

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History of PV/T (LCA and economic studies)

Economic aspects on PV/T systems are given by Leenders et al (2000), while the environmental impact of PV modules by using the Life Cycle Assessment (LCA) methodology has been extensively used at University of Rome "La Sapienza". Frankl et al (2002) presented LCA results on the comparison of PV/T systems with standard PV and thermal systems, confirming the environmental advantage of PV/T systems.

LCA results for PV/T collectors (Tripanagnostopoulos et al, 2005, 2006) are compared with standard PV modules for the positive environmental impact for low temperature heating of water or air PV/T collectors.

The application of PV/T systems in the industry is suggested as a viable solution for wider use of solar energy systems (Battisti and Tripanagnostopoulos, 2005).

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History of PV/T (use in industry and agriculture)

Some other works on PV/T systems are referred to TRNSYS results (Kalogirou and Tripanagnostopoulos, 2007) and to the PV/T absorbers with linear Fresnel lenses, for integration on building atria or greenhouses, aiming to achieve solar control in illumination and temperature of the interior space, providing also electricity and heat (Tripanagnostopoulos et al, 2007).

New designs of PV/T devices were suggested for heating of water and air (Tripanagnostopoulos, 2007, Assoa et al, 2007), some others to be coupled with heat pumps (Jie et al, 2008), to achieve cost effective desiccant cooling (Beccali et al, 2009) and to agricultural applications (Garg et al, 1991, Sopian et al, 2000, Othman et al , 2006, Rocamora and Tripanagnostopoulos, 2006, Nayak and Tiwari, 2008 and Kumar and Tiwari, 2010).

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History of PV/T (commercial models)

Commercial PV/T collectors are few and the market is still at the ground level. For concentrating PV/T collectors, some steps have been done for operation at higher temperatures and some commercial CPV/T collectors have been introduced in the market.

The first commercial PV/T model, which has been introduced in the market was the Multi Solar System (MSS) from Millenium Electric, which is a flat type PV/T collector for water and air heating.

Other commercial flat type PV/T collectors are Twinsolar (Grammer), Solar, SolarVenti (Aidt Miljo), TIS (Secco Sistemi), SolarDuct (SolarWall), PVTWIN, SES, Solimpeks, Solarhybrid, etc.

Concentrating PV/T collectors (CPVT), are products of Heliodynamics, Arontis (Absolicon), Power-Spar, ZenithSolar, Cogenra, Menova, etc.

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PVT/WATER collectors

Multi Solar System, MSS Millenium Electric, Israel

ΤΕΣ PV/T SOLAR WATER HEATING SYSTEM

CPC Hybrid PV/T – WATER solar collectors

RenOn : PV cells attached on thermal absorber

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PVT/AIR collectors

Twinsolar (Grammer)

SolarWall

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Absolicon

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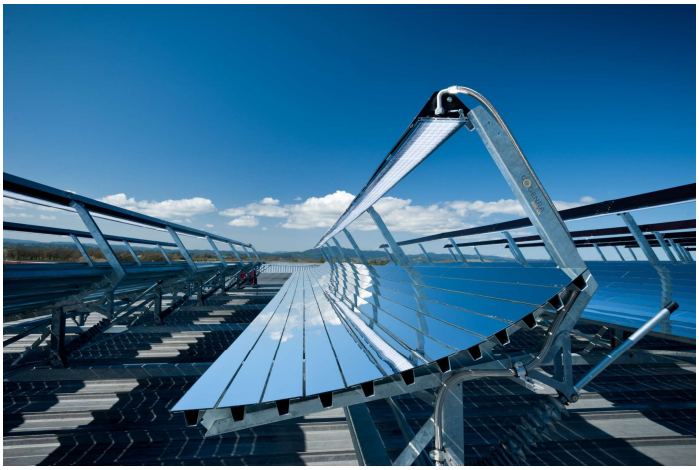

cogenra

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Design aspects of PV/T

In PV/T, the cost of the thermal unit is the same irrespective if the PV module is c-Si, pc-Si or a-Si. Thus the relative cost of the thermal unit per PV area cost is different and almost double for a-Si compared to c-Si or pc-Si PV modules.

The complete PV/T systems include the necessary additional components (BOS, for the electricity and the BOS for the heat) and therefore the final energy output is reduced due to the electrical and thermal losses from one part to the other.

Aiming to establish criteria for PV/T collector standards and certification, Kramer and Helmers (2013) have recently introduced basic aspects. In addition, the study of Dupeyrat et al (2014) gives interesting results for a new PV/T collector design.

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Design aspects of PV/T

PV/T collectors can adapt energy load with limitations in availability of external building surface, as for zero energy buildings. Aelenei and Goncalves (2014), give a figure of PV/T application to the achievement of zero energy buildings.

Regarding the thermal part of PV/T collectors, the active efficiency is less than that of the typical solar thermal collectors, because the suppression of thermal losses has limitations regarding the electrical part of the PV/T collector.

The PV/T systems that use typical PV modules and provide heat above 80° C have lamination problems, due to the high operating temperatures and need further development.

Some improvements in PV module encapsulation and construction, aiming to swift thermal insulation and suffer operating temperatures higher than 80° C, have been recently presented by Fortuin et al (2014).

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Design aspects of PV/T

The prediction of the operating temperature of PV module is complicated and several formulas have been suggested (Lasnier and Ang, 1990, Skoplaki et al 2008, Skoplaki and Palyvos, 2009, Tripanagnostopoulos et al, 2005, 2006).

An additional cover to PV modules increases PV/T thermal performance, but decreases electrical output, because of the absorbed and reflected away solar radiation and the electrical efficiency reduction due to higher temperature.

In façade/tilted roof mounted PV/T systems the thermal protection increases system thermal efficiency, but the lower thermal losses keep PV temperature at higher level, reducing electrical efficiency. For effective BIPV cooling of PVT collectors, passive cooling with PCM can be used (Aelenei et al, 2014).

Among PV/T review papers are the works of Charalambous et al (2007), Zondag (2008), Chow (2010), Tripanagnostopoulos (2012) and Ibrahim et al, 2011 and the material on PV/T collectors in the web-site of IEA-SHC/Task 35 (2005).

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Design aspects of PV/T

The flat type PV/T solar systems can be used in the domestic and in the industrial sectors, mainly for preheating water or air and to feed Heat Pumps with electricity and heat, to increase their COP.

In PV/T-air systems, ambient air is directly heated by PV panels, while in the PV/T-water systems, the thermal contact is through a heat exchanger.

PV/T solar collectors integrated on building roofs and facades can replace separate thermal collectors and photovoltaics.

These new solar devices can be used to residential buildings, hotels, hospitals and other buildings, to cover agricultural and industrial energy demand and also to provide simultaneously electricity and heat in several other sectors.

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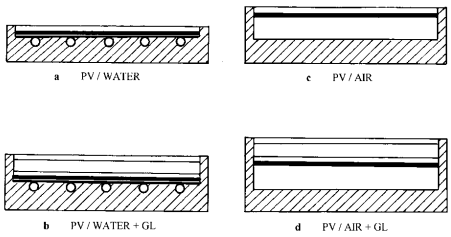
Design aspects of PV/T



(Tripanagnostopoulos et al, 2002)

To increase system operating temperature, an additional glazing is used, but it decreases the absorbed solar radiation and therefore PV module electrical output, because the incoming solar radiation is reduced due to absorption by the glazing and reflection from it, depending on the angle of incidence.

For water heat extraction, the water can circulate through pipes in contact with a flat sheet, placed in thermal contact with PV module rear surface.

In PV/T systems the thermal unit, the necessary fan or pump and the external ducts or pipes for fluid circulation constitute the complete system.

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Design aspects of PV/T

In most industrial processes, electricity for the operation of motors and other machines and heat for water, air or other fluid heating and for physical or chemical processes, are necessary.

This makes hybrid PV/T systems promising devices for an extended use adapting industrial applications (washing, cleaning, pasteurizing, sterilizing, drying, boiling, distillation, polymerization, etc).

In the agricultural sector, typical form or new designs of PV/T collectors can be used as transparent cover of greenhouses and applied for drying and desalination processes, providing the required heat and electricity.

Hybrid PV/T systems can be also applied to buildings combined with geothermal, biomass or wind energy. In combination with photovoltaics, small wind turbines can provide also electricity and cover effectively the load.

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Design aspects of PV/T

The combination of concentration devices with PV modules is a viable method to reduce system cost, replacing the expensive cells with a cheaper solar radiation concentrating system to achieve higher efficiencies at effective PV temperatures.

The concentrating PV/T systems (CPVT) use reflective (mirrors) and refractive (lenses) optical devices and are characterized by their concentration ratio C (or CR). Concentrating PV/T (CPVT) systems consist of tracking flat reflectors, parabolic trough reflectors, Fresnel lenses and dish type reflectors, combined with PV/T receivers.

CPVT systems with medium or high CR values require PV modules that suffer temperatures up to 150 ^{o}C or more, to produce steam, or to adapt processes in higher temperatures .

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Design aspects of PV/T

Life Cycle Assessment (LCA) methodology and cost analysis for typical PV and PV/T systems confirm their environmental advantage compared to standard PV modules (Tripanagnostopoulos et al, 2005, 2006).

TRNSYS methodology and other modeling methods can be used, to get a clear idea about practical aspects, including their cost effectiveness (Kalogirou, 2001).

PVT Roadmap (2006), the European guide for the development and market introduction of PV-Thermal technology, is a basic brochure that provides information for this solar technology.

Task 35 of the International Energy Agency (IEA-SHC/Task35) has performed studies on the technology and application of PV/T systems.

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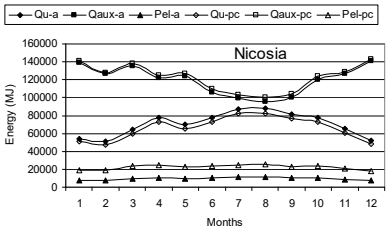
Design aspects of PV/T

A TRNSYS simulation for industrial process heat of 60° C and 80° C of PV/T collectors, is the work of Kalogirou and Tripanagnostopoulos (2007), applying pc-Si and a-Si PV panels.

The electrical production of pc-Si PV panels is more than a-Si PV panels, but the solar thermal contribution is lower.

A non-hybrid PV system produces about 25% more electrical energy but the present system covers also a large percentage of the thermal energy of the industry considered.

Although a-Si PV modules are much less efficient than pc-Si PV modules, they give better economic figures due to their lower initial cost, thus they have better cost/benefit ratio.



Monthly useful, auxiliary and electrical energy of the 80° C load temperature industrial process heat system for Nicosia. (Kalogirou and Tripanagnostopoulos, 2007)

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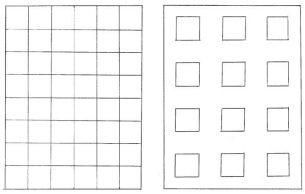
Design aspects of PV/T

Convectional PV/T solar collectors usually consist of two parts, the solar radiation absorbers and the heat extraction units.

The fraction of absorber plate area covered by PV cells is given in terms of cells packing factor, *PF*. The *PF* is defined as the fraction of the area occupied by the cells to the total module surface area.

In partially filled PV/T systems, the spaces between rows of cells allow incident solar radiation to pass through and get absorbed directly by the secondary absorber plate (Aste et al, 2003).



packing factor (PF) of pasted cells (100% left, 25% right).

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Design aspects of PV/T

The PF in PV/T systems is selected either for electrical load (electrical priority operation, EPO) or thermal load (thermal priority operations, TPO) (Fujisawa and Tani 1997).

The EPO has higher packing factor (PF$\geq$ 0.7), hence the electrical power is optimized while the TPO has lower packing factor hence optimized for thermal production.

PV cells are of higher cost compared to other PV/T components and thus a priority is given to the electrical power.

TPO is affected by the direct absorption of solar radiation that passes through inter-cells spacing and increases the heat extraction from the back of cells. Thus, *PF* determines the ratio of electricity to heat and characterizes the practical use of PV/T modules.

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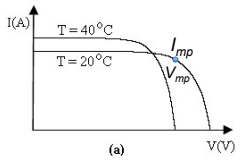
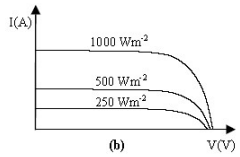
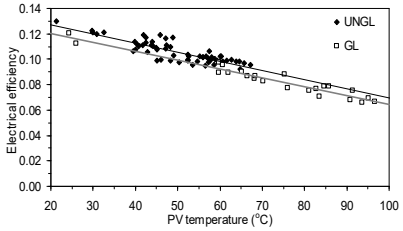
PV/T energy performance

V_{oc}, open circuit voltage
I_{sc}, short circuit current
V_{mp} maximum voltage
I_{mp} maximum current
MPP: maximum power: $P_{max} = I_{mp} * V_{mp}$
Incident solar radiation: $Pin = Ir * A\,a$
Fill factor, $FF= (I_{mp} * V_{mp})/ (I_{sc} * V_{mp})$
Electrical efficiency: $\eta el = P_{max}/ Pin$
Thermal efficiency: $\eta th = Q_u/ Qin$
$Qu = mCp(To-Ti)$
$Qin= Ir*Aa$
electrical efficiency $n_{el} = P_{max}/ Pin$
thermal efficiency $n_{th} = Qu/Qin$
total conversion efficiency
n_t: $n_{t} = n_{el} + n_{th}$







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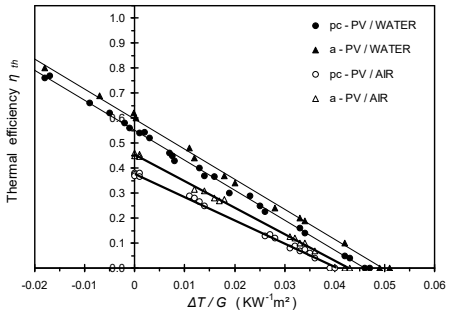
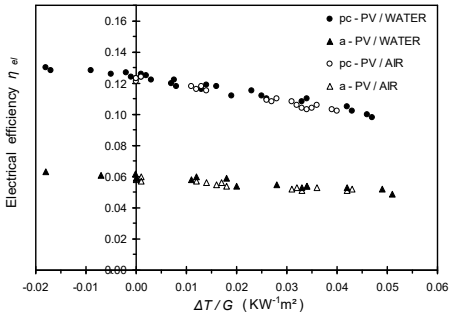
PV/T energy performance





(Tripanagnostopoulos et al, 2002)

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PV/T energy performance

Formula to calculate pc-Si and c-Si PV module temperature as function of ambient temperature T_a and solar radiation G (Lasnier and Ang, 1990):

$T_{PV}=30+0.0175(G-300)+1.14(T_a-25)$

Formula for a-Si PV modules, as their lower electrical efficiency results to slightly higher PV module temperature compared to pc-Si PV modules.

$T_{PV}=30+0.0175(G-150)+1.14(T_a-25)$

In PV/T systems PV temperature depends also on the system operating conditions and mainly on heat extraction fluid mean temperature. PV electrical efficiency η_{el} can be function of $(T_{PV})_{eff}$, which corresponds to the PV temperature for the operating conditions of PV/T systems.

$(T_{PV})_{eff}=T_{PV}+(T_{PV/T}-T_a)$

The operating temperature $T_{PV/T}$ of PV/T system corresponds to PV module and to thermal unit temperatures and can be determined approximately by the mean fluid temperature. This modified formula corresponds to the increase of PV operating temperature due to the reduced heat losses to the ambient.

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PV/T-WATER systems

$$Q_s = Q_u + Q_L + Q_{OL} + Q_{el}$$

$$Q_s = A_{pv} G$$

$$Q_u = n_{th} A_{pv} G$$

$$Q_{OL} = (1-(\tau\alpha)) A_{pv} G$$

$$Q_{el} = n_{el} A_{pv} G$$

$$\eta_{th} = \dot{m} c_p (T_o - T_i) / A_\alpha G$$

$$\Delta T / G \qquad \Delta T = T_i - T_\alpha$$

$$\eta_{el} = I_m V_m / A_\alpha G$$

$$U_L = U_t + U_b + U_e$$

$$\overline{U}_L = U_L - \tau\alpha\eta_{ref}\beta_{ref} G$$

$$\eta_{el} = \eta_{ref}\left(1-\beta_{ref}(T_{pv}-T_{ref})\right)$$

$$n_{th} = \frac{Q_u}{A_c G}$$

$$Q_u = A_c\left[S - U_L\left(T_{p,m} - T_a\right)\right]$$

$$Q_u = A_c F_R\left[S - U_L\left(T_i - T_a\right)\right]$$

The steady state efficiency modified by Florschuetz (1979) for PV/T collectors

$$n_{th} = \overline{F_R}\left[\tau\alpha\left(1-n_{pv}\right) - \overline{U_L}\left(\frac{T_{wi}-T_a}{G}\right)\right] = \frac{mC_p\left(T_{wo}-T_{wi}\right)}{A_c G}$$

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PV/T –AIR systems

For the PV/T-air collector, efficiency factor F is calculated from the modified equation from Duffie and Beckman (1991):

$$\overline{F}' = \left[1 + \frac{\overline{U}_L (h_c + h_r)}{h_c^2 + 2h_c h_r}\right]^{-1}$$

where h_c and h_r are the convective and radiative heat transfer coefficients in the air duct. The relationship to determine heat removal efficiency F is given by Florschuetz (1979) as:

$$\overline{F}_R = \frac{\dot{m}C_p}{A_{pv}\overline{U}_L}\left[1 - \exp\left(-\frac{A_{pv}\overline{U}_L \overline{F}'}{\dot{m}C_p}\right)\right]$$

where ***m*** and C_p are air flow rate and specific heat capacity of air. The steady-state thermal efficiency of the PV/T-air collector is calculated from the measured data from:

$$\eta_{th} = \frac{\dot{m}C_p (T_{out} - T_{in})}{A_a G}$$

The forced convection heat transfer coefficient in the air channel is assumed constant for all channel walls . In case of short length PV/T modules (≈ 1 m), the correlation of Tan and Charters (1969) can be used (which includes the effect of thermal entrance length of the air duct) to compute Nusselt number hence forced convection heat-transfer coefficient. Reynolds number Re and hydraulic diameter are determined from their usual expressions and Prandtl number Pr is usually 0.7 for air.

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PV/T –AIR systems

The pressure drop is derived by applying Bernoulli's law and energy equation (with assumptions of Esposito, 1998). For forced flow, the driving force is provided by the pump which does some work by pushing air through the pump head H_p.

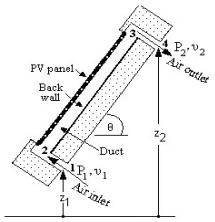
The opposing forces are represented by the total head loss H_L which includes major losses due to friction between channel walls and air stream represented by friction head H_f and the minor losses caused by any obstruction that hinders smooth flow of air from inlet to outlet, evaluated as the product of loss coefficient k_i and available velocity head. The head loss is then given as the sum of major and minor losses:

The loss coefficients k_i for PV/T-air collector include the effect of entrance, exit and the two 90° turns inside the channels and loss coefficients at these four places give the total loss coefficient *k* (Young et al ,1997). The major head loss H_f is determined from the Darcy-Weisbach equation (Esposito, 1998):

$f = 64\mathrm{Re}^{-1}$ Laminar flow

$f = 0.316\mathrm{Re}^{-0.25}$ Turbulent flow

$$H_f = \frac{\upsilon^2}{2g} f\left(\frac{L}{D_H}\right)$$



(Tonui and Tripanagnostopoulos, 2007, 2008)

$$H_p = H_L = H_f + \sum_i k_i \frac{\upsilon^2}{2g}$$

The pressure drop ΔP is

$$\Delta P = g\rho H_P$$

The electrical power required also depends on the fan efficiency η_{fan} and the motor efficiency η_{motor} and the power required P is given by:

$$P = \frac{\dot{m}\Delta P}{\rho} = \frac{\dot{m}\Delta P}{\rho \eta_{fan} \eta_{motor}}$$

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PV/T –AIR systems

The expression for the induced air flow rate by natural convection in steady-state analysis is based on Bernoulli's equation from inlet (location 1) to outlet (location 4) of the airflow channel

$$P_1 + \frac{\rho_1 \upsilon_1^2}{2} + \rho_1 g z_1 - \frac{fL}{D_H}\frac{\upsilon^2}{2} - k_1\frac{\rho_1\upsilon_1^2}{2} - (k_2+k_3)\frac{\rho\upsilon^2}{2} = P_2 + \frac{\rho_2\upsilon_2^2}{2} + \rho_2 g z_2 + k_4\frac{\rho_2\upsilon_2^2}{2}$$

Considering simplifying assumptions both vents at inlet (1) and outlet (2) are open to the atmosphere hence $P_1 = P_2$ and inlet ambient air is considered as an infinite reservoir with negligible velocity, hence ≈ 0, (Esposito, 1998). Considering these assumptions, the above equation is reduced to:

$$\rho_1 g z_1 - \rho_2 g z_2 = \frac{\rho_2\upsilon_2^2}{2} + \frac{fL}{D_H}\frac{\rho\upsilon^2}{2} + (k_2+k_3)\frac{\rho\upsilon^2}{2} + k_4\frac{\rho_2\upsilon_2^2}{2}$$

The buoyancy term is derived for one-dimensional "fictitious loop analysis" for naturally ventilated buildings (Ibarahim et al, 1999, Brinkworth et al, 2000) and using the expression for buoyancy term from these references it becomes:

$$(\rho_1 - \rho_2) g L \sin\theta = \frac{\rho_2\upsilon_2^2}{2} + \frac{fL}{D_H}\frac{\rho\upsilon^2}{2} + (k_2+k_3)\frac{\rho\upsilon^2}{2} + k_4\frac{\rho_2\upsilon_2^2}{2}$$

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PV/T –AIR systems

The parameter D_H is the hydraulic diameter of the air duct and equals four times the cross-sectional area of the duct divided by the wetted perimeter. The continuity equation and the simplified relationship between temperature and density (Boussinesq approximation) are given respectively by:

$$\dot{m} = \rho A_{ch}\upsilon = \rho_2 A_2 \upsilon_2 \qquad \rho_T = \rho\beta T$$

where A_{ch} and A_2 are channel and exit vent areas respectively, is the density of air at any temperature T and $\beta = 1/T_f$, with $T_f = (T_{in} + T_{out})/2$.

$$\beta L g \sin\theta (T_{out} - T_{in}) = \frac{\upsilon^2}{2}\left[\frac{fL}{D_H} + \beta T_{out}(1+k_4)\left(\frac{A_{ch}}{A_2}\right)^2 + (k_2+k_3)\right]$$

$$\upsilon^2 = 2g\beta L\sin\theta(T_{out} - T_{in})\left[2.2 + \frac{fL}{D_H} + 2\beta T_{out}\left(\frac{A_{ch}}{A_2}\right)^2\right]^{-1} \qquad Q_u = \dot{m} C_p (T_{out} - T_{in}) = \eta_{th} A_{pv} G$$

$$\dot{m}^2 = 2g\beta L\sin\theta(A_{ch}\rho)^2(T_{out} - T_{in})\left[2.2 + \frac{fL}{D_H} + 2\beta T_{out}\left(\frac{A_{ch}}{A_2}\right)^2\right]^{-1}$$

$$\dot{m} = \left(\frac{2g\beta(A_{ch}\rho)^2 A_{pv}\eta_{th} GL\sin\theta}{C_p\left[2.2 + fL/D_H + 2\beta T_{out}(A_{ch}/A_2)^2\right]}\right)^{\frac{1}{3}} \qquad Gr = \frac{L^3\rho^2 g\beta\Delta T}{\mu} \qquad h_c = \frac{k}{D_H}\mathrm{Nu}$$

$$\mathrm{Nu}_L = 1.2\,Ra^{1/3} \qquad \mathrm{Nu}_L = 0.378\,Ra^{1/4}$$

$$f = 1.906(\mathrm{Gr}/\mathrm{Pr})^{1/12}$$ Laminar flow

$$f = 1.368(\mathrm{Gr}/\mathrm{Pr})^{1/11.9}$$ Turbulent flow

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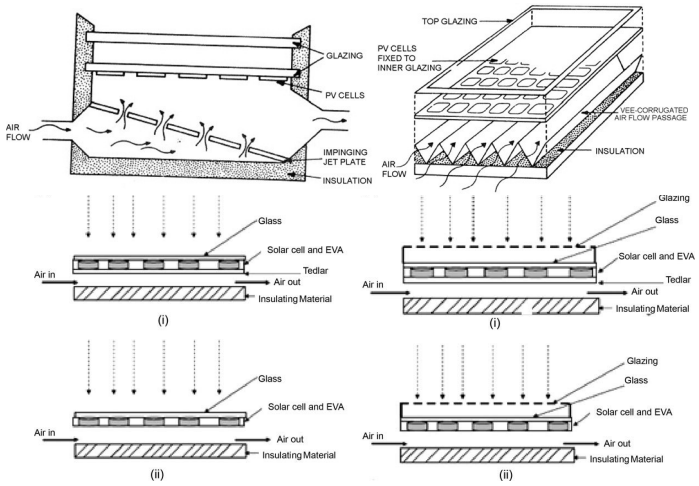

(Tiwari and Sodha, 2006)

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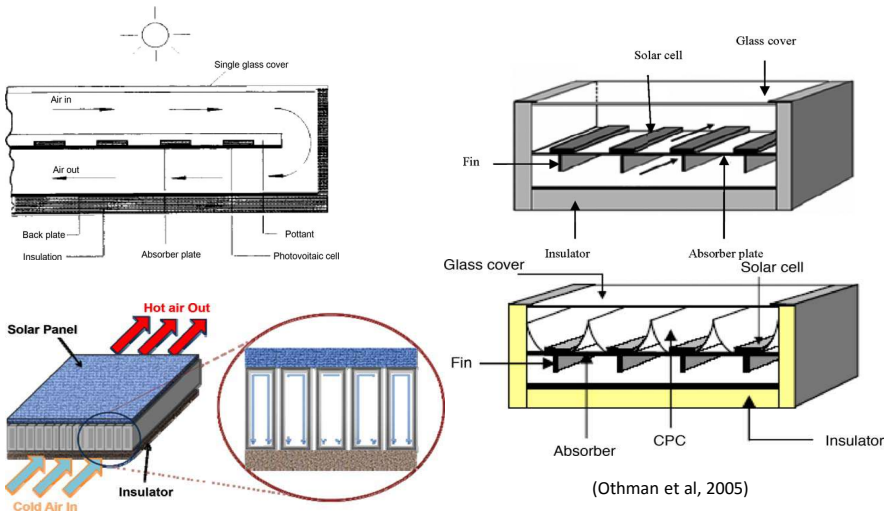

(Othman et al, 2005)

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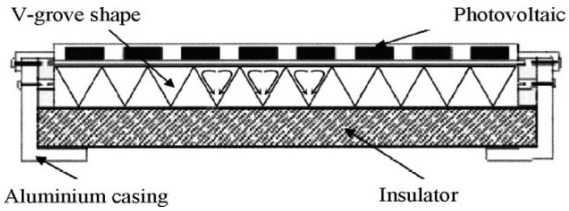

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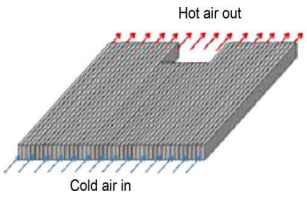

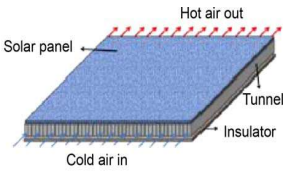

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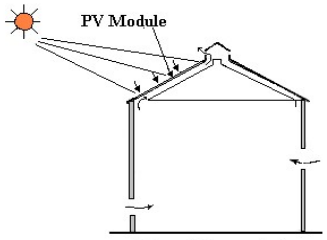
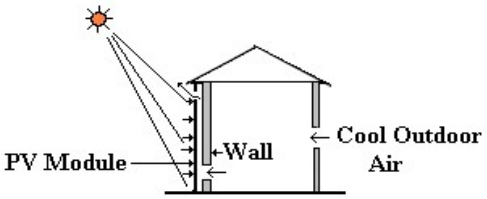
PV/T –AIR systems



PV module mounted as a Solar Roof Ventilato



PV mounted on Facade for Ventilation

For PV module mounted on the roof, fresh air enters into building through open (or infiltration) windows and doors and achieves natural ventilation. PV modules integrated on the façade with air gap, contribute to effective heat flow of circulating air out of the building. PV/T system can be used as "ventilation driver" for natural ventilation of building creating substantial ventilation rate. TMS "shields'' the back wall from undesirable heat transmission.

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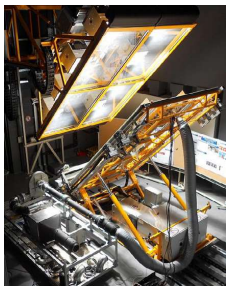
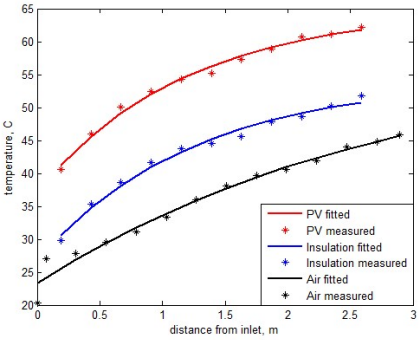
PV/T –AIR systems





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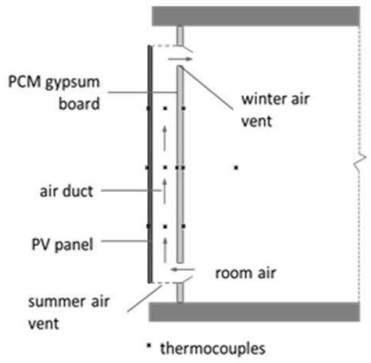

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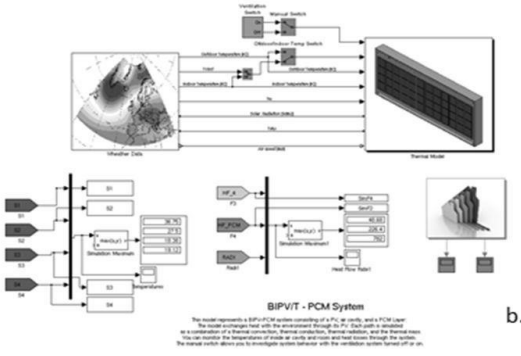

b.

(Aelenei et al, 2014)

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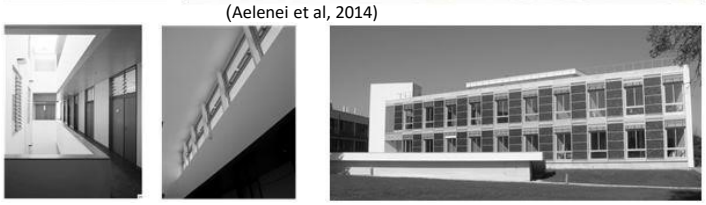
PV/T –AIR systems

(Aelenei et al, 2014)



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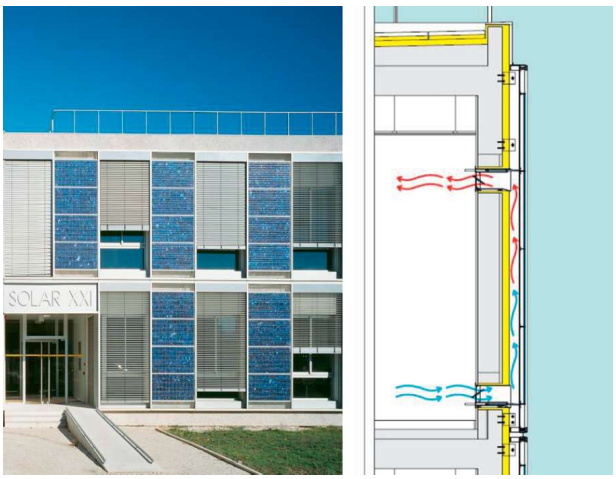
PV/T –AIR systems



(Aelenei et al, 2014)

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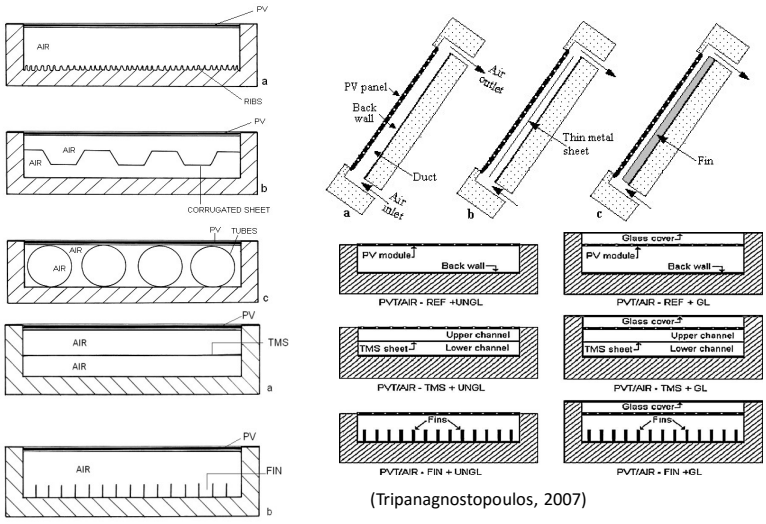
Modified PV/T systems



(Tripanagnostopoulos, 2007)

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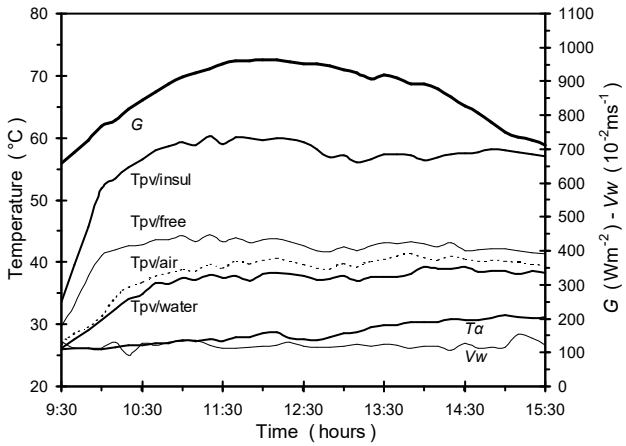
Daily test results of PV and PV/T systems



PVT/water: water cooled PV module

PVT/air: air cooled PV module

PV/free: thermal losses from both PV sides

PV/insul: thermally insulated PV rear side

(Tripanagnostopoulos et al, 2002)

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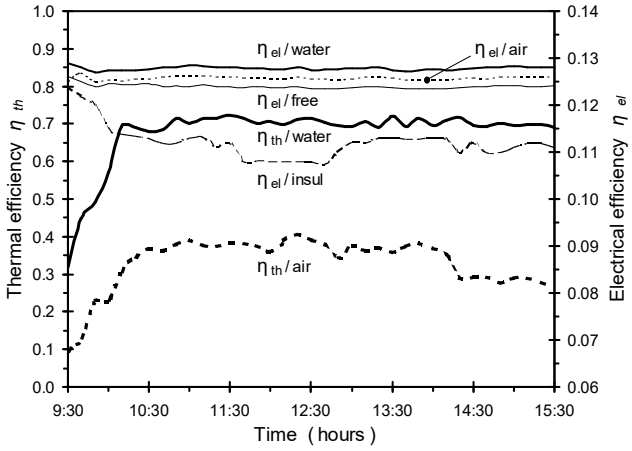
Daily test results of PV and PV/T systems



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End of the 1st part of lecture on PV/T collectors

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